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ELMOE: AN IBM-704 PROGRAM
TREATING ELASTIC SCATTERING RESONANCES
IN FAST REACTORS

by

A. L. Rago and H. H. Hummel

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ABSTRACT

A description of the operations carried out by the ELMOE code is given. This code carries out MUFT-type calculations for dealing with the elastic scattering resonances of the light elements present in fast reactors. Sources of information for the cross-section library in current use with the program, input specification, and operating instructions are also given.

I. INTRODUCTION

Elastic scattering resonances in the light elements present in fast power reactors have always been troublesome since they cause rapid fluctuations in the scattering cross sections of these materials, whereas variations of cross sections of fissile and fertile materials in the fast region are comparatively slow. The change in the neutron leakage and flux caused by adding or removing the light materials is difficult to calculate exactly, because the elastic moderation introduced by these materials causes perturbation of the neutron energy spectrum in the vicinity of the resonances.

In order to deal more effectively with problems of this type, an IBM-704 code, ELMOE, has been prepared. This code calculates the Fourier transform of the neutron flux for a mixture of moderators heavier than hydrogen, with the moderator-scattering law rigorously taken into account. Approximations available in the flux calculations are the usual P-1 and "consistent" P-1 and B-1 [1-3]. This code thus performs approximately the same calculation for moderators heavier than hydrogen as that which the MUFT codes [4] carry out for hydrogen. Although designed specifically for fast-reactor calculations, it can also be applied to thermal and intermediate reactors. No special provisions have yet been incorporated for dealing with capture resonances, however. Applications of the program have been previously reported [5-7].

A feature of the code is that certain parameters which are slowly varying need be specified only for "coarse" groups which are much wider in energy than the "fine" groups used to take detailed account of elastic moderation. This greatly reduces the amount of input data required.

The coarse groups are those ordinarily used in fast-reactor calculations with a total of 10 to 20 groups spanning the fast region. A fine-group structure is superimposed over all or a part of the usual groups. Associated with each of the fine groups is a set of Legendre polynomial expansion coefficients of the scattering cross section of each element. The original intention was that the fine-group network be fine enough to trace out the detailed variation of each scattering cross section. This has proved practicable except for the high-resolution data of Hibdon [8-10] for scattering from sodium, which are being specially handled as described later. From the Legendre polynomial expansion coefficients, elastic-transfer, transport, and elastic-removal cross sections for the light elements are calculated for each fine group. Fission, capture, and inelastic-removal cross sections are normally kept constant for the fine groups corresponding to a given coarse group. Variable capture cross sections for the fine groups may be supplied if desired. Inelastic transfers entering the fine groups are distributed in proportion to the fine-group energy widths. The fission source has an energy dependence of the form $\sqrt{E} e^{-E/T}$ within the coarse groups. A variable fission source for the fine groups may be supplied if desired. No provision is made for inelastic transfers within coarse groups.

The fine groups all have the same lethargy width. Meshing of the coarse and fine groups is accomplished by a slight redefinition of the coarse-group energy limits. Although the fine-group lethargy width is arbitrary, in practice the labor involved in changing it except by integral multiples is such that only one width (and in some cases twice this width) has so far been used.

At least one coarse group at the top and bottom of the energy range must be handled in the usual way, i.e., not subdivided. Otherwise the fine-group region may cover any desired part of the energy spectrum. The groups not subdivided are calculated according to the usual equations for the Fourier transform.

II. CALCULATION OF CROSS SECTIONS

1. Elastic-scattering Cross Sections

It is assumed in the calculation that data on the angular dependence of the elastic-scattering cross sections in the center-of-mass system are presented in the form

$$\sigma_{sc}(\omega') = \sum_{\ell} B_{\ell} P_{\ell}(\mu'), \quad (\text{II-1})$$

where

$\sigma_{sc}(\omega')$ = cross-section scattering into the solid angle element $d\omega'$,

μ' = cosine of the scattering angle in the center-of-mass system,

P_{ℓ} = ℓ th Legendre polynomial.

Data in the laboratory system are converted to the center-of-mass system. In the laboratory system the fractional energy change per collision is related to μ' by [1].

$$\frac{E}{E_0} = \frac{1}{(1+A)^2} (A^2 + 1 + 2A\mu'),$$

or

$$\mu' = 1 - \frac{2}{\alpha} \left(1 - \frac{E}{E_0} \right), \quad (\text{II-2})$$

where

$$\alpha = 4A/(A+1)^2,$$

A = moderator mass number,

E_0 = initial energy of the neutron.

Integrating the scattering cross section over azimuth angle, one obtains

$$2\pi \sigma_{sc}(\omega') d\mu' = \sigma_{sc}(E_0 \rightarrow E) dE. \quad (\text{II-3})$$

Upon differentiating Eq. (II-2) and substituting this in Eq. (II-3) we obtain

$$\sigma_{SC}(E_0 \rightarrow E) dE = \frac{4\pi}{E_0 \alpha} dE \sum_{\ell} B_{\ell} P_{\ell}(\mu'). \quad (\text{II-4})$$

Let

$$x = \frac{1}{\alpha} \left(1 - \frac{E}{E_0} \right).$$

Then, combining Eqs. (II-2) and (II-4), one may evaluate the Legendre polynomials in terms of:

$$P_1(\mu') = \mu' = 1 - 2x;$$

$$P_2(\mu') = \frac{1}{2} (3\mu'^2 - 1) = 1 - 6x + 6x^2;$$

$$P_3(\mu') = \frac{1}{2} (5\mu'^3 - 3\mu') = 1 - 12x + 30x^2 - 20x^3;$$

$$P_4(\mu') = \frac{1}{8} (35\mu'^4 - 30\mu'^2 + 3) = 1 - 20x + 90x^2 - 140x^3 + 70x^4.$$

Therefore, x varies from 0 to 1 as E varies from E_0 , the initial energy, to $E = (1 - \alpha) E_0$, the minimum possible final energy. This range is divided into n intervals chosen so that the ratio r of lower to upper energy for the interval is the same for each interval, i.e.,

$$r = E_j / (E_{j-1}).$$

Therefore

$$x_0 = 0;$$

$$x_1 = \frac{1}{\alpha} (1 - r);$$

$$x_2 = \frac{1}{\alpha} (1 - r^2);$$

.

$$x_n = \frac{1}{\alpha} (1 - r^n) = 1;$$

$$r = (1 - \alpha)^{1/n}.$$

If one now integrates Eq. (II-4) over the final energy interval $(E_{\ell}, E_{\ell-1})$ corresponding to the x -interval $(x_{\ell-1}, x_{\ell})$,

$$\int_{E_\ell}^{E_{\ell-1}} \sigma_{sc}(E_0 \rightarrow E) dE = -4\pi \int_{x_{\ell-1}}^{x_\ell} dx \left[\sum_{\ell=0}^4 B_\ell P_\ell(\mu') \right]. \quad (\text{II-5})$$

Collecting terms x_ℓ^{i+1} and denoting the coefficients as A_i ,

$$\sigma_{eltr}^{E_0 \rightarrow \ell} = 4\pi \left[A_0^0 (x_\ell - x_{\ell-1}) + A_1^0 \frac{(x_\ell^2 - x_{\ell-1}^2)}{2} + A_2^0 \frac{(x_\ell^3 - x_{\ell-1}^3)}{3} + A_3^0 \frac{(x_\ell^4 - x_{\ell-1}^4)}{4} + A_4^0 \frac{(x_\ell^5 - x_{\ell-1}^5)}{5} \right],$$

(II-6)

where

$\sigma_{eltr}^{E_0 \rightarrow \ell}$ = microscopic elastic-scattering cross section from energy E_0 to Group ℓ ;

B_ℓ^0 = coefficients of the Legendre polynomial expansion at energy E_0 ;

$$A_0^0 = B_0^0 + B_1^0 + B_2^0 + B_4^0;$$

$$A_1^0 = 2B_1^0 - 6B_2^0 - 12B_3^0 - 20B_4^0;$$

$$A_2^0 = 6B_2^0 + 30B_3^0 + 90B_4^0;$$

$$A_3^0 = -20B_3^0 - 140B_4^0;$$

$$A_4^0 = 70B_4^0.$$

If one now lets E_0 range over E_j , $j = 0, \dots, J$, the entire range under consideration, and ℓ range over the interval $k = 1, \dots, J$, where

$$k = j + \ell,$$

and

$$E_j = \text{lower energy limit of Group } j,$$

then, for the general case,

$$\sigma_{eltr}^{E_j \rightarrow k} = 4\pi \left[A_0^j (x_{k-j} - x_{k-j-1}) + A_1^j \frac{(x_{k-j}^2 - x_{k-j-1}^2)}{2} + A_2^j \frac{(x_{k-j}^3 - x_{k-j-1}^3)}{3} + A_3^j \frac{(x_{k-j}^4 - x_{k-j-1}^4)}{4} + A_4^j \frac{(x_{k-j}^5 - x_{k-j-1}^5)}{5} \right].$$

The elastic-scattering cross section from Group j to Group k is calculated from

$$\sigma_{\text{eltr}}^{j \rightarrow k} = \frac{\sigma_{\text{eltr}}^{E_j \rightarrow k} + \sigma_{\text{eltr}}^{E_{j-1} \rightarrow k}}{2}.$$

2. Elastic-removal Cross Sections

The elastic-removal cross section from energy E_j to below E_{j+1} may be represented as

$$\sigma_{\text{elr}}^{E_j, E_{j+1}} = \sum_{k=j+2}^{j+n} \sigma_{\text{eltr}}^{E_j \rightarrow k}.$$

Substituting from Eq. II-6 we get

$$\sigma_{\text{elr}}^{E_j, E_{j+1}} = 4\pi \left[A_0^j (1 - x_1) + A_1^j \frac{(1 - x_1^2)}{2} + A_2^j \frac{(1 - x_1^3)}{3} + A_3^j \frac{(1 - x_1^4)}{4} + A_4^j \frac{(1 - x_1^5)}{5} \right]. \quad (\text{II-7})$$

The elastic-removal cross section from Group j is calculated as

$$\sigma_{\text{elr}}^j = \frac{1}{2} \left(\sigma_{\text{elr}}^{E_{j-1}, E_j} + 4\pi B_0^j \right).$$

3. Transport Cross Sections

The transport cross section is given by

$$3\sigma_{\text{tr}}^{E_j} = 3\sigma_{\text{sc}}^{E_j} (1 - \bar{\mu}) + 3\sigma_a, \quad (\text{II-8})$$

where

$\bar{\mu}$ = average scattering angle cosine in laboratory system,

σ_a = total removal cross section due to processes other than elastic scattering.

$$\sigma_{\text{sc}}^{E_j} = 4\pi B_0^j.$$

From Eq. (II-8),

$$3\sigma_{tr}^{E_j} = 12\pi B_0^j \left(1 - \frac{2}{3A} - u_{1,1}^{-1} \frac{B_1^j}{3B_0^j} - u_{1,2}^{-1} \frac{B_2^j}{3B_0^j} - u_{1,3}^{-1} \frac{B_3^j}{3B_0^j} - u_{1,4}^{-1} \frac{B_4^j}{3B_0^j} \right) + 3\sigma_a,$$

or

$$3\sigma_{tr}^{E_j} = 4\pi \left(3B_0^j - \frac{2B_0^j}{A} - u_{1,1}^{-1} B_1^j - u_{1,2}^{-1} B_2^j - u_{1,3}^{-1} B_3^j - u_{1,4}^{-1} B_4^j \right) + 3\sigma_a,$$

where $u_{1,1}^{-1}$, $u_{1,2}^{-1}$, $u_{1,3}^{-1}$ and $u_{1,4}^{-1}$ are elements of the transformation matrix $U^{-1}[1]$ transforming the B_ℓ from the center-of-mass system to the laboratory system. As above, the cross section at Group j is calculated by

$$3\sigma_{tr}^j = \frac{3\sigma_{tr}^{E_j} + 3\sigma_{tr}^{E_{j-1}}}{2} + 3\sigma_a.$$

III. FLUX APPROXIMATIONS

There are four flux approximations available as options in ELMOE. The equations are given below.

1. P-1 Approximation

For the P-1 approximation, the equation for the flux in the k^{th} group is

$$\phi_k^i = \frac{\beta_k + \psi_k}{\frac{B_i^2}{3\Sigma_{\text{tr}}^k} + \Sigma_a^k + \Sigma_{\text{elr}}^k}, \quad (\text{III-1})$$

where

ϕ_k^i = i^{th} iterate of the flux group k ;

β_k = fraction of fission source in group k (assumed same for all isotopes);

$\psi_k = \sum_{j=1}^{k-1} (\Sigma_{\text{eltr}}^{j \rightarrow k} + \Sigma_{\text{intr}}^{j \rightarrow k}) \phi_j^i$ = scattering source from higher energies;

$\Sigma_{\text{eltr}}^{j \rightarrow k}$ = elastic-scattering transfer cross section, group j to group k ;

$\Sigma_{\text{intr}}^{j \rightarrow k}$ = inelastic-scattering transfer cross section, group j to group k ;

Σ_a^k = absorption (total non-elastic removal) cross section for group k ;

Σ_{elr}^k = elastic-removal cross section for group k ;

Σ_{tr}^k = transport cross section for group k ;

B_i^2 = the i^{th} iterate of the buckling.

This equation is calculated by iteration until convergence on B^2 , which is decided by

$$\left| \sum_{k=1}^N \nu_k \Sigma_k^f \phi_k^i - 1 \right| \leq \epsilon, \quad (\text{III-2})$$

where

$\nu_k \Sigma_k^f$ = neutrons per fission times fission cross section for group k , and

ϵ = convergence criterion for iterative s

In the further discussion, the superscript "i" is dropped as a convergence is assumed.

2. B-1 Approximation

If one now replaces Σ_{tr}^k in Eq. (III-1) by $\gamma_k \Sigma_{tr}^k$, where γ_k is defined as

$$\gamma_k = \frac{\alpha_k \tan^{-1} \alpha_k}{3 \left(1 - \frac{\tan^{-1} \alpha_k}{\alpha_k} \right)}; \quad \alpha_k = \frac{B}{\Sigma_{tr}^k},$$

one obtains the B-1 approximation [2]. Under this transformation, Eq. (III-1) becomes

$$\phi_k = \frac{\beta_k + \psi_k}{\frac{B^2}{3\gamma_k \Sigma_{tr}^k} + \Sigma_a^k + \Sigma_{elr}^k},$$

and the iterative procedure used in the P-1 approximation is used for solution.

3. "Consistent" P-1 Approximation

In the ordinary P-1 approximation, the angular distribution of the slowing-down source is not properly taken into account. The equations correctly taking it into account in the P-1 approximation are given in [1] as Eqs. (11.31a) and (11.31b). For simplicity, these are given here with spatial variation in the Z direction only assumed.

$$\frac{1}{4\pi} \frac{\partial J(E, Z)}{\partial Z} \int_0^\infty \phi(E', Z) S_0(E' \rightarrow E) dE' - \frac{\Sigma_{tot}(E)\phi(E, Z)}{4\pi} + S_{00}(E, Z), \quad (III-3)$$

$$\frac{1}{4\pi} \frac{\partial \phi(E, Z)}{\partial Z} = \int_0^\infty J(E', Z) S_1(E' \rightarrow E) dE' - \frac{3\Sigma_{tot}(E)J(E, Z)}{4\pi}, \quad (III-4)$$

$J(E, Z)$ = current,

$\phi(E, Z)$ = flux,

$4\pi S_{00}(E, Z)$ = inelastic-scattering plus fission sources (assumed isotropic).

For the Fourier transform one can set

$$J(E, Z) = -iJ(E)e^{iBZ}, \quad (III-5a)$$

$$\phi(E, Z) = \Phi(E)e^{iBZ}, \quad (\text{III-5b})$$

and

$$S_{00}(E, Z) = S_{00}(E)e^{iBZ}. \quad (\text{III-5c})$$

In multigroup notation, with E' and E corresponding to groups j and k , respectively,

$$S_0(E' \rightarrow E) \rightarrow S_0^{j \rightarrow k} = \frac{1}{4\pi} \Sigma_{\text{eltr}}^{j \rightarrow k}$$

and

$$S_1(E' \rightarrow E) \rightarrow S_1^{j \rightarrow k} = \frac{1}{4\pi} \frac{3}{2} \left(\frac{E_k}{E_j} \right)^{1/2} \left[(A + 1) - \frac{(A - 1)}{E_k/E_j} \right] \Sigma_{\text{eltr}}^{j \rightarrow k}.$$

E_j and E_k may be taken as the lower group limits:

$$J(E) \rightarrow J_k,$$

$$\phi(E) \rightarrow \phi_k.$$

Writing Eq. (III-3) in multigroup form with the use of Eq. (III-5),

$$BJ_k = \sum_{j=k-n}^{k-1} \phi_j \left[\Sigma_{\text{eltr}}^{j \rightarrow k} + \Sigma_{\text{intr}}^{j \rightarrow k} \right] - (\Sigma_a^k + \Sigma_{\text{elr}}^k) \phi_k + \beta_k. \quad (\text{III-6})$$

Equation (III-4) can be similarly rewritten as

$$\frac{J_k}{B} = \frac{\phi_k}{3\Sigma_{\text{tot}}^k} + \frac{1}{3\Sigma_{\text{tot}}^k} \sum_{j=k-n}^{k-1} \frac{J_j}{B} \frac{3}{2} \left(\frac{E_k}{E_j} \right)^{1/2} \left[(A + 1) - \frac{(A - 1)}{E_k/E_j} \right] \Sigma_{\text{eltr}}^{j \rightarrow k}, \quad (\text{III-7})$$

and we define

$$\Sigma_{\text{tot}}^k = \Sigma_{\text{tr}}^k + \bar{\mu}_k \Sigma_{\text{elr}}^k.$$

Solving Eqs. (III-6) and (III-7) for the flux, one obtains

$$\phi_k = \frac{\beta_k + \sum_{j=k-n}^{k-1} \phi_j [\Sigma_{\text{eltr}}^{j \rightarrow k} + \Sigma_{\text{intr}}^{j \rightarrow k}] - \frac{1}{3\Sigma_{\text{tot}}^k} \sum_{j=k-n}^{k-1} \frac{3}{2} \left(\frac{E_k}{E_j} \right)^{1/2} BJ_j \left[(A + 1) - (A - 1)E_k/E_j \right] \Sigma_{\text{eltr}}^{j \rightarrow k}}{\frac{B^2}{3\Sigma_{\text{tot}}^k} + \Sigma_a^k + \Sigma_{\text{elr}}^k} \quad (\text{III-8})$$

Equations (III-7) and (III-8) are a coupled set which are solved iteratively to obtain the group fluxes and currents, and the eigenvalue B^2 .

4. "Consistent" B-1 Approximation[2, 3]

If one substitutes $\gamma_k \Sigma_{tot}^k$ for Σ_{tot}^k , where γ_k is defined as

$$\gamma_k = \frac{\alpha_k \tan^{-1} \alpha_k}{3 \left(1 - \frac{\tan^{-1} \alpha_k}{\alpha_k} \right)}, \quad \alpha_k = \frac{B}{\Sigma_{tot}^k}, \quad (\text{III-9})$$

one obtains the "consistent" B-1 approximation, in which a rigorous solution for the Fourier transform is obtained except that only a P-1 expansion of the scattering cross sections in the laboratory system is used. For this case, Eqs. (III-7) and (III-8) are transformed to

$$\frac{J_k}{B} = \frac{\phi_k}{3 \gamma_k \Sigma_{tot}^k} + \frac{1}{3 \gamma_k \Sigma_{tot}^k} \sum_{j=k-n}^{k-1} \frac{J_j}{B} \frac{3}{2} \left(\frac{E_k}{E_j} \right)^{1/2} \left[(A+1) - (A-1)(E_k/E_j) \right] \Sigma_{eltr}^{j \rightarrow k} \quad (\text{III-10})$$

and

$$\phi_k = \frac{\beta_k + \sum_{j=k-n}^{k-1} \phi_j \left[\Sigma_{eltr}^{j \rightarrow k} + \Sigma_{intr}^{j \rightarrow k} \right] - \frac{1}{3 \gamma_k \Sigma_{tot}^k} \sum_{j=k-n}^{k-1} \frac{3}{2} \left(\frac{E_k}{E_j} \right)^{1/2} B J_j \left[(A+1) - (A-1)(E_k/E_j) \right] \Sigma_{eltr}^{j \rightarrow k}}{\frac{B^2}{3 \gamma_k \Sigma_{tot}^k} + \Sigma_a^k + \Sigma_{elr}^k} \quad (\text{III-11})$$

Again, the solution involves coupling Eqs. (III-10) and (III-11), with iteration on B^2 .

For each of these approximations when the convergence criterion is satisfied, the code calculates a flux-weighted average of the fine-group cross sections to get an average homogenized coarse-group cross-section set. The coarse-group transport cross section is averaged for each of the options as follows:

P-1

$$\overline{3\Sigma}_{tr} = \frac{\sum \phi / 3 \Sigma_{tr}}{\sum \phi},$$

B-1 and Consistent B-1

$$\overline{D} = \frac{\sum J/B}{\sum \phi},$$

$$\overline{3\Sigma}_{tr} = \frac{3B}{\tan \frac{\bar{D}B}{(1+\bar{D})}},$$

Consistent P-1

$$\bar{D} = \frac{1}{\overline{3\Sigma}_{tr}} = \frac{\sum J/B}{\sum \phi}.$$

These averaged cross sections are then used to do a normal fundamental mode calculation, using diffusion theory for the P-1 and Consistent P-1 cases, and the asymptotic solution to the transport equation for the B-1 and Consistent B-1 cases.

IV. TREATMENT OF NARROW RESONANCES

The ratio of final to initial fine-group energies thus far being used is 0.99133, so that at 100 keV the group width is 0.87 keV and at 200 keV 1.74. Since many of the resonances in sodium reported by Hibdon [8] in this energy region have widths less than 1 keV, this group spacing cannot be used to describe such resonance shapes. The method of dealing with these very narrow resonances is as follows. First, a problem is run with the low-resolution data for sodium given in [12], which can be adequately traced out with the group spacing being used. The usual assumption of the narrow-resonance approximation is made: that over one of the fine groups the total source is constant and equal to that calculated with the low-resolution data. For the P-1 approximation the actual magnitude of the source for each group need not be known. In this case the assumption is made that the source S equals $\phi(E) \Sigma_{\text{tot}}(E)$ within the fine group. An average transport cross section for fine groups is obtained from

$$\frac{1}{\Sigma_{\text{tr}}^j} = \frac{\int_{E_{j-1}}^{E_j} \frac{dE}{\Sigma_{\text{tot}}(E) \Sigma_{\text{tr}}(E)}}{\int_{E_{j-1}}^{E_j} \frac{dE}{\Sigma_{\text{tot}}(E)}}.$$

$\Sigma_{\text{tot}}(E)$ and $\Sigma_{\text{tr}}(E)$ are obtained from the detailed sodium data, with the contributions of material other than sodium being held at the values for the original ELMOE calculation. Finally, the values of $1/\Sigma_{\text{tr}}^j$ are weighted with the fluxes from the ELMOE calculation to obtain a revised coarse-group value.

To obtain a corrected scattering cross section for elastic-removal calculation, the following integral is computed:

$$\sigma_{sNa}(j) = \frac{\int_{E_{j-1}}^{E_j} \frac{\sigma_{sNa}(E)dE}{\Sigma_{\text{tot}}(E)}}{\int_{E_{j-1}}^{E_j} \frac{dE}{\Sigma_{\text{tot}}(E)}}$$

These values of $\sigma_{sNa}(j)$ are used in conjunction with the original ELMOE fluxes to obtain a corrected elastic-removal cross section for sodium. A library tape containing $\sigma_{sNa}(E)$ is available for this calculation.

V. LIBRARY TAPE

As mentioned above, the elastic-scattering-matrix calculation uses the coefficients B_L in the expression

$$\sigma(\theta_c) = \sum_L B_L P_L(\cos \theta_c),$$

where $\sigma(\theta_c)$ is the differential scattering cross section per unit solid angle in the center-of-mass system. The coefficients B_L are supplied to the program by means of a library tape. The first file of the library tape contains the multigroup cross-section sets. The coefficients B_L comprise the second file. The multigroup cross-section sets are described below (Section VI).

The coefficients may be supplied in either laboratory or center-of-mass system, and the ratio of the coefficient to the $L = 0$ coefficient may be supplied if desired. All coefficients are converted to be stored in the center-of-mass system on the library tape.

The library currently contains coefficients for the following isotopes: carbon, oxygen, sodium, sodium-1, sodium-2, aluminum, vanadium, chromium, iron, Type 304 stainless steel, Hastelloy, nickel and niobium.

Sodium-1 coefficients were obtained by doing an ELMOE calculation for a typical metal core and then using the narrow-resonance option from 66 keV to 830 keV, and using the re-averaged total scattering cross section for sodium output from this procedure as the basis for new values of B_0 for sodium-1 in this range. The higher B_L in this range were kept at the same ratio as for sodium. Sodium-2 coefficients were obtained in the same manner except that the ELMOE calculation was for an oxide core. Type 304 stainless steel coefficients are simply linear combinations of those for iron, chromium, and nickel with volume fractions by weight of 0.72, 0.19, and 0.09 respectively. Hastelloy coefficients were constructed in a similar manner, with the composition assumed to be 0.22 iron, 0.24 chromium, and 0.54 nickel, molybdenum being neglected. Total cross-section data were taken [12] and [13]. Total cross sections of sodium for the detailed treatment by the narrow-resonance approximation (Section IV) were taken from [8-10]. Since high-resolution angular-distribution data are available for only a few isolated resonances, the procedure followed was to derive the coefficient of the isotropic term from total cross-section data and to take the ratio of coefficients corresponding to higher values of L to the $L = 0$ coefficient from the angular-distribution data. Sources of angular-distribution and inelastic-scattering data were as follows:

Sodium

In the energy range 200-800 keV the data of [14] were used. Outside this range up to 1400 keV, [15] was used. Above 1400 keV, ω_1 was based on $\bar{\mu} = \omega_1/3\omega_0$ given in Fig. 22 of [16], where the ω 's are defined by

$$\sigma_s(\theta) = \frac{\sigma_s}{4\pi} \sum_L \omega_L P_L(\cos \theta),$$

in which

θ = scattering angle in the laboratory system,

σ_s = total scattering cross section.

The quantities ω_2 and ω_3 were obtained by linear extrapolation to 1.49 and 0.61, respectively, at 3.7 MeV. This was based on data in [17] for sulphur. Total scattering cross sections were obtained by subtracting the inelastic-scattering cross sections of [18] from the total cross-section data.

Aluminum

The same procedure was followed in this case as for sodium, except that the only angular-distribution data available below 1400 keV were, and are, those of [15]. Inelastic-scattering cross sections were taken from [19].

Iron, Nickel, Chromium

The data of [15] were used up to 1800 keV for ω_1 , ω_2 , ω_3 , and ω_4 . ω_1 to 3.7 MeV was obtained from $\bar{\mu}$ in [16]. ω_2 , ω_3 , and ω_4 were obtained by linear extrapolation to 2.02, 1.77, and 1.10, respectively, at 3.7 MeV, this point being based on the data in [17]. Inelastic-scattering cross sections were those of [19].

Carbon

In the energy range from 0 to 2.2 MeV the data of [20] were used, whereas in the range from 2.2 to 3.7 MeV the data of [21] were employed.

Oxygen

In the energy range from 0 to 1.7 MeV the data of [20] were used, where above this to 3.7 MeV the data in [22] were used.

Niobium and Vanadium

In the range from 0 to 1.35 MeV the data of [15] were used. Above 1.35 MeV, ω_1 was based on $\overline{\mu}$ given in [16]. Coefficients for higher values of L have not yet been supplied above 1.35 MeV.

The available library of coefficients clearly leaves much to be desired. The energy resolution of the cross-section data, particularly of the angular-distribution data, is in general not nearly as good as one would like to have. The necessity of using angular-distribution data of resolution differing widely from the total cross-section data is not very satisfactory. In some cases, the total cross section obtained in the angular-distribution measurements is clearly inconsistent with the other total cross-section data from transmission measurements, even taking into account the difference of resolution. A better estimate of high-energy angular distribution than that made here could undoubtedly be obtained by means of the optical model of the nucleus. Since the library was prepared in 1960, it does not include data available later than that except for those of [9] and [10].

A library tape containing more detailed data for sodium due to Hibdon [8-10] is utilized by the narrow sodium-resonance routine. Energy vs. total scattering cross section for sodium are given for the range from 60 to 832 keV in increments of 0.1 and 0.2 keV.

VI. INPUT

The coarse-group cross sections are taken from one of a library of such sets available. These may be either in the form used in the REX code [23] or in that of the SNG code [24]. Elastic-removal cross sections for the light elements used in these sets must be supplied, as they are subtracted out. The Legendre polynomial expansion coefficients for the light elements may be supplied either in the center-of-mass or the laboratory system. The library of such coefficients currently available includes the following elements: Fe, Ni, Cr, Nb, V, Al, Na, Na-1, Na-2, C, O, stainless steel, and Hastelloy.

The number of fine groups that can be used is limited by the 32K-core storage. If more groups than this limit are desired, the problem is run in more than one pass, subdividing different energy regions with an overlap of at least one or two coarse groups to produce a proper elastic moderation source at the upper end of the subdivided region. The number of fine groups that can be used is a function of the maximum size of the elastic scattering matrix. The Legendre coefficient library currently in use corresponds to elastic-scattering matrices of order 20, 29, and 39 for sodium, oxygen, and carbon, respectively. When sodium, oxygen, or carbon is the lightest element present, the maximum number of fine groups that can be used in the ordinary P-1 calculation is 880, 682, and 535, respectively. With the consistent calculations, the corresponding values are 535, 393, and 303.

Materials in a problem that require Legendre coefficients for cross-section evaluation are referred to as "light" elements. Those that do not are referred to as "heavy." A feature of ELMOE allows problems to be done in "sets." A "set" is defined as a group of problems that differ only in composition (value of volume fraction). For the set only one calculation of the elastic-scattering matrix is executed, effecting a considerable time saving.

Description of the Input

ELMOE Calculation

Card	FORTRAN	Format	Definition
Set No.	Symbol		
1	IDB	(13I4,E12.5)	Identification of Legendre coefficient set required from Library Tape.
	IDX		Identification of macroscopic cross section set required from Library Tape.

Card Set No.	FORTRAN Symbol	Format	Definition
	MEND		Number of heavy elements, ≤ 19 .
	MTOT		Number of light elements, $1 \leq MTOT \leq 20$, $MTOT + MEND \leq 20$.
	JEND		Number of fine groups. For limit see NW1.
	MH		Order of Legendre expansion used for differential scattering cross section, ≤ 5 .
	KM2		If Δ is lethargy increment of Legendre library, problem lethargy increment is $(KM2)\Delta$.
	KMIN		Initial coarse group subdivided.
	KEND		Final coarse group subdivided.
	IT = 1		
	KT = 1		
	ITH = 1		
	NW1		Determines maximum size of scattering matrix ($JEND \times N$) (See Card Set No. 5) NW1 = 1 IOPT = 1,2 (880 x 20) NW1 = 2 IOPT = 1,2 (682 x 29) NW1 = 3 IOPT = 1,2 (545 x 39) NW1 = 4 IOPT = 3,4 (535 x 20) NW1 = 5 IOPT = 3,4 (393 x 29) NW1 = 6 IOPT = 3,4 (303 x 39)
	EO		Energy in keV of the top of group KMIN.
2		(18I4)	
	KRSEC(1),KRSEC(2),..., KRSEC(MEND + MTOT)		Indicates position in cross-section set of materials used in problem.
3		(18I4)	
	KRSET(1),KBSET(2),..., KBSET(MTOT)		Indicates position in Legendre coefficient set of materials used in problem.
4		(12A6)	
	ID		Problem identification. Column 1 blank, 2-72, alphanumeric characters.

Card Set No.	FORTRAN Symbol	Format	Definition
5		(18I4)	
	IOPT		Flux approximation. IOPT = 1 P-1. IOPT = 2 B-1. IOPT = 3 "Consistent" P-1. IOPT = 4 "Consistent" B-1.
	IA		Output options. IA = 1 Normal. IA = 2 Fine-group elastic-removal cross section printed out for each light material. IA = 3 Fine-group elastic-scattering matrix and elastic-removal cross section printed out for each light material.
	IC		IC = 1 Fine-group output omitted. IC = 2 Fine-group output printed. Input options.
	ID		ID = 1 Fine-group capture cross section not supplied as input. ID = 2 Fine-group capture cross section supplied as input.
	IE		IE = 1 Fine fission source not supplied as input. IE = 2 Fine fission source supplied as input.
	IF		Preliminary sodium NR treatment option. IF = 1 Normal. IF = 2 Preliminary problems for sodium narrow-resonance treatment.
	NM		Position in problem of sodium.
	N		Maximum energy loss per collision of sodium (in groups).
	NTIMES		Number of problems in set.

Card Set No.	FORTRAN Symbol	Format	Definition
6	(18I4)		
	NUM(KMIN), ..., NUM(KEND)		Number of fine groups in standard groups subdivided.
7	(6E12.5)		
	A(1),AC(1), $U_{11}^{-1}(1), U_{12}^{-1}(1),$ $U_{13}^{-1}(1), U_{14}^{-1}(1),$... A(MTOT), AC(MTOT), $U_{11}^{-1}(MTOT),$ $U_{12}^{-1}(MTOT),$ $U_{13}^{-1}(MTOT),$ $U_{14}^{-1}(MTOT)$		Atomic weight, atoms/cc, transformation vector [11] from CMS to LAB system for material 1.
	A(MTOT+1), AC(MTOT+1) ... A(MTOT+MEND), AC(MTOT+MEND)		Atomic weight, atoms/cc, transformation vector from CMS to LAB system for last light material.
8	(6E12.5)		
	EPS,BBO,V(1), ..., V(MTOT+MEND)		Atomic weight and atoms/cc for first heavy material.
			Atomic weight and atoms/cc for last heavy material.
9	If IE = 2 KU,KL, $\beta(KU),$... $\beta(KL)$	(2I4/(6E12.5))	Convergence criteria, initial buckling guess, volume fractions for material 1 through MTOT+MEND.
10	If ID = 2 LL	(I4)	Fine-group limits of specification, followed by the fission source for these fine groups.
		(4I4/(6E12.5))	
	$M^1, K^1, KU^1, KL^1,$ $\sigma_c^1(KU),$... $\sigma_c^1(KL)$		Material number (position in problem), coarse group, fine-group limits within coarse group, and capture cross sections for batch 1.

Card Set No.	FORTRAN Symbol	Format	Definition
10		(4I4/(6E12.5))	
	$M^{LL}, K^{LL}, KU^{LL}, KL^{LL},$ $\sigma_c^{LL}(KU), \dots, \sigma_c^{LL}(KL)$		Material number, coarse group, fine-group limits within coarse group, and capture cross sections for batch LL.
11	If NTIMES > 1		Repeat card set numbers 4 and 8-10 for each problem in set.

Note: If attempting to iterate on the buckling with a non-multiplying medium, a negative input buckling guess must be given.

Treatment for Sodium Narrow Resonances

Card Set No.	FORTRAN Symbol	Format	Definition
1	blank card		Sentinel to tape-monitor routine.
2	ID	(72X)	Title card. Column 1 blank.
3		(3I4)	
	KMIN		First-group narrow-resonance treatment is performed.
	KEND		Last-group narrow-resonance treatment is performed.
	KD		Output option.
			KD = 1 Fine-group-averaged total scattering and transport cross section printed out.
			KD = 2 Fine-group-averaged total scattering and transport cross section not printed out.

Note: Problems run on the sodium narrow-resonance routine may be run only one at a time, i.e., not more than one to a set.

To Add Cross-section Sets to Library Tape

Card Set No.	FORTRAN Symbol	Format	Definition
1		(2I4)	
	IDB	=0	
	IDX	non-zero	
2		(I1,6I5)	
	KNUM	=0	Add to existing tape.
		=1	Start new tape.
	IDNUM		Cross-section set identification.
	ME		Number of materials in cross-section set, ≤ 20 .
	KAN		Number of inelastic-scattering groups, ≤ 23 .
	KMAX		Number of energy groups, ≤ 24 .
	IRS		Cross-section format option =1 REX cross-section format. =2 SN cross-section format.
	KSET		Number of cross-section sets being added to tape at this time.

3 Cross-section deck

The SN cross-section cards contain eight words per card with a blank column between words. Column one always contains a nine punch and the sign of the number is placed over the "one-tenth's" digit, thereby designating the position of the decimal point. The cross sections are written in the following order:

Col. 1	9 punch
Col. 2-9	$\nu\sigma_{f,j}$
Col. 11-18	$\sigma_{tr,j}$
Col. 20-27	$\sigma_{tr,j} - \sigma_{a,j}$
Col. 29-36	$\sigma_{in}(j-1 \rightarrow j)$
Col. 38-45	$\sigma_{in}(j-2 \rightarrow j)$
...	
	$\sigma_{in}(j-L \rightarrow j)$

where L = total number of inelastic-scattering groups for the cross-section set and $j=1, 2, \dots, J$ (the group index). The cards are arranged groupwise for each material and the fission spectrum (β_j) precedes the cross-section data.

Card Set No.	FORTRAN Symbol	Format	Definition
4		(9E8.6)	
	$\sigma_{elr}^{1,1}$		Elastic-removal cross section for group 1, material, through material ME.
	\dots		
	$\sigma_{elr}^{1,ME}$		
	$\sigma_{elr}^{KMAX,1}$		Elastic-removal cross section for group KMAX, material 1 through material ME.
	\dots		
	$\sigma_{elr}^{KMAX,ME}$		Each group starts a new card.
5	If KSET > 1	5I5	
	IDNUM		Cross-section set identification.
	ME		Number of materials in set, ≤ 20 .
	KAN		Number of inelastic-scattering groups, ≤ 23 .
	KMAX		Number of energy groups, ≤ 24 .
	IRS		=1 REX cross-section format =2 SN cross-section format

Repeat card set numbers 3 and 4 with card set number 5 for each KSET-1 sets.

To Add Legendre Coefficient Set to Library Tape

Card Set No.	FORTRAN Symbol	Format	Definition
1		(I4)	
	IDB		Non-zero
2		(I5)	
	NTOT		Number of Legendre coefficient sets already on library tape.
3		(4I5,2E12.5)	
	KBNUM		Set identification (consecutive order).
	MAT1		Number of material.
	IGP1		Number of energy levels.

Card Set No.	FORTRAN Symbol	Format	Definition
3	MADP		=1 Add complete set. =2 Add MAT1 materials to set KBNUM. =3 Add IGPI energy level following existing levels to set KBNUM. =4 Add IGPI energy levels preceding existing levels of set KBNUM.
	EEO1		Energy of first level being added to set KBNUM.
	U1		Constant energy ratio of set, E_i/E_{i-1} .
4	(6E12.5)		
	A(1), ..., A(MAT1)		Atomic weight of materials, in order of increasing weight.
5	(18I4)		
	IB ¹ ,IW ¹ (1),IG1 ¹ (1),IG2 ¹ (1), ..., IW ¹ (IB),IG1 ¹ (IB),IG2 ¹ (IB)		Number of batches of coefficients of different format for material 1, fol- lowed by the batch format and batch energy-level limits.
	...		IW(1)=1 Coefficients in CMS
	...		IW(I)=2 Coefficients in CMS ratio, B_0 , B_1/B_0 , B_2/B_0 , B_3/B_0 , B_4/B_0 .
			IW(I)=3 Coefficients in LAB ratio, A_0 , A_1/A_0 , A_2/A_0 , A_3/A_0 , A_4/A_0 .
			IW(I)=4 Coefficients in LAB system.
	IB ^{MAT1} ,IW ^{MAT1} (1), IG1 ^{MAT1} (1),IG2 ^{MAT1} (1), ..., IW ^{MAT1} (IB),IG1 ^{MAT1} (IB), IG2 ^{MAT1} (IB)		Number of batches of coefficients of different format for material MAT1, followed by the batch format and batch energy-level limits. Each material starts a new card.

In addition, a BCD tape to be mounted on logical unit 4 containing the following information must be prepared.

Data	Remarks
$A_0(1,1), A_1(1,1), A_2(1,1), A_3(1,1), A_4(1,1)$	Legendre coefficients for material 1, energy level 1. FORMAT (5E12.5).
$A_0(1,IGP1), A_1(1,IGP1), A_2(1,IGP1),$ $A_3(1,IGP1), A_4(1,IGP1)$	Legendre coefficients for material 1, energy level IGP1. FORMAT (5E12.5).
$A_0(MAT1,IGP1), A_1(MAT1,IGP1), A_2(MAT1,IGP1),$ $A_3(MAT1,IGP1), A_4(MAT1,IGP1)$	Legendre coefficients for material MAT1, energy level IGP1. FORMAT (5E12.5).

VII. OUTPUT

On-line Output

The code prints out the iteration number, buckling, square root of the buckling, and K_{eff} at each iteration, both for the ELMOE and coarse-group fundamental-mode calculations.

Off-line

The off-line output consists of a summary of the input, initial, and final values of the buckling, and material-dependent-averaged coarse-group elastic-removal cross sections. Also, for each coarse group the flux, current/B, the diffusion coefficient, and elastic-removal cross section are listed. For each fine group the following quantities are normally written: flux, current/B (except for P_1), slowing-down density, inelastic source, and elastic source. The complete transfer matrix can be obtained on option. For further clarification of the output, the following comments hold.

Material-dependent elastic-removal cross sections are the partial contribution from material i to the homogenized-averaged coarse-group elastic-removal cross section.

Coarse-group Output

$1/D$ - average value $3\sigma_{tr}$ homogenized for all materials
 Elastic removal - sum of elastic transfers out of the coarse group divided by the total coarse-group flux
 Absorption - averaged homogenized value of $(\sigma_{abs} - \sigma_{elr})$ for light elements and σ_{abs} for heavy elements.

Fine-group Output

Slowing-down density at E is the total number of neutrons slowing down below E because of elastic collisions above E . "A" denotes the source from higher energies due to elastic scattering. "B" denotes the source from higher energies due to inelastic scattering. "C" denotes the contribution from the current term in the "consistent" case.

Finally, a HOBO [25] equivalent is done; it is a coarse-group fundamental-mode calculation using averaged homogenized cross sections from the ELMOE calculation. The buckling obtained should be the same as for the main ELMOE calculation unless an error has occurred. The summary of macroscopic cross sections obtained has proven very useful. For the $P-1$ option the information summarized in the HOBO equivalent output is written on the output tape with a "Q" control character causing

the information to be punched on cards. These cards may then be used (preceded by a title card) for input to an independent routine that provides a calculation of the adjoint flux.

Code Tape

The code tape itself consists of the following records, each preceded by WBTSB 2 - Absolute Binary Tape Loaders:

1. Monitor
2. Cross-section tape-reading routine
3. Legendre coefficient tape-reading routine
4. Cross-section tape-writing routine
5. Legendre coefficient tape-writing routine
6. Sodium narrow-resonance treatment
7. Scattering-matrix calculation
8. Fundamental-mode calculation
9. Output routine

Routines 7, 8, 9 are repeated for each of the dimension limits mentioned above. The code tape is written with the WB-CTB 2 - Absolute Binary Card to tape routine. To make the code tape, READY the card deck in the card reader, CLEAR, and depress LOAD CARDS. The code tape is written on logical unit 1.

VIII. OPERATING INSTRUCTIONS

The code requires a 32K IBM 704 with 7 on-line tape units, an on-line printer, and an on-line card reader. The card reader uses the standard share 72 x 72 board, and the printer the SHARE number 2 board.

SENSE SWITCHES. All sense switches are to be in the "up" position.

Tape Units.

Tape 1 ELMOE Code
Tape 2 ELMOE Library
Tape 3 Scratch
Tape 4 Scratch, or BCD Input for Legendre coefficient writing routine.
Tape 5 Preliminary for sodium narrow resonance routine
(used only for preliminary to sodium narrow resonance routine or narrow resonance routine)
Tape 7 Binary input for sodium narrow resonance routine
(library supplied)
Tape 10 Output tape

Running procedure

1. Mount and ready tapes
2. Underflow switch on
3. All sense switches up
4. Ready cards in reader
5. Ready printer
6. Clear, depress LOAD TAPE.

Program stops on card reader select. Write EOF on tape 10, rewind and print on Program Control. STOPS: FORTRAN program stops.

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APPENDIX

Sample Problem

The following information is given for a sample problem:

1. Input sheets
2. List of materials in cross-section set
3. List of materials in Legendre coefficient set
4. On-line output
5. Off-line output.

704 INPUT DATA

FORM II

COST CODE

PROGRAM RE 196

PROBLEM ELMOE

ORIGINATOR A. RAGO

DATE 23 Aug

PAGE 2 OF 3

1	2	3	4	5	6	7	8
1 2 3 4 5 6 7 8 9	0 1 2 3 4 5 6 7 8 9	0 1 2 3 4 5 6 7 8 9	0 1 2 3 4 5 6 7 8 9	0 1 2 3 4 5 6 7 8 9	0 1 2 3 4 5 6 7 8 9	0 1 2 3 4 5 6 7 8 9	0 1 2 3 4 5 6 7 8 9
.0 1 1 8 1 4 1		.0 1 1 9 1 7 1		.0 1 2 1 1 2 1		.0 1 2 1 2 1 6 1	
.5		.6 5 1		.7 9 1		.8 4 1	
1 1 1 2 3 1		1 1 1 4 8 1		1 1 1 6 1 7 1		2 1 1 4 1	
2 1 1 7 1 8 1		1 1 1 7 1 8 1		1 1 1 0 3 1		1 1 1 0 3 1	
.0 2 1 1 4 1		.0 1 1 5 1 9 1		.0 1 1 2 7 1		.0 0 9 8 1	
.0 0 0 7 1 1 1		.0 0 6 4 1		.0 0 6 1		.0 0 5 6 1	
.0 0 0 4 6 1		.0 0 4 5 1		.0 0 4 4 1		.0 0 4 3 1	
.0 0 3 9 1		.0 0 3 8 1		.0 0 3 7 1		.0 0 3 6 1	
.0 0 3 3 1		.0 0 3 2 1		.0 0 3 1 1		.0 0 3 0 1	
.0 0 2 8 5 1		.0 0 2 8 1		.0 0 2 7 8 1		.0 0 2 7 6 1	
.0 0 2 7 1		.0 0 2 6 8 1		.0 0 2 6 6 1		.0 0 2 6 4 1	
.0 0 2 5 8 1		.0 0 2 5 6 1		.0 0 2 5 4 1		.0 0 2 5 2 1	
.0 0 2 4 7 1		.0 0 2 4 7 1		.0 0 2 4 7 1		.0 0 2 4 7 1	
.0 0 2 4 7 1							
S I A M P I L E	I P I O I B I L E	M I N I O I	1 2 1				
.0 0 0 0 0 0 1	.0 0 2 1 1				.0 3 1 2 1		.0 0 3 3 1
							.0 1 5 2 5 1
1 1 1 1 1		.0 1 1 4 0 4 1		.0 0 1 1 5 6 1			
1 1 3 1	1 5 1 1 3 9 1 3	4 7 1 1 1					
1 0 1 1 8 1 4 1		.0 1 1 9 1 7 1		.0 1 2 1 1 2 1		.0 1 2 1 2 1 6 1	
1 5 1 1 1		.0 1 6 5 1 1 1		.7 1 9 1 1		1 8 1 4 1	
1 2 3 4 5 6 7 8 9	0 1 2 3 4 5 6 7 8 9	0 1 2 3 4 5 6 7 8 9	0 1 2 3 4 5 6 7 8 9	0 1 2 3 4 5 6 7 8 9	0 1 2 3 4 5 6 7 8 9	0 1 2 3 4 5 6 7 8 9	0 1 2 3 4 5 6 7 8 9
	1	2	3	4	5	6	8

704 INPUT DATA

FORM II

COST CODE

PROGRAM RE 196

PROBLEM ELMOE

ORIGINATOR A. RAGO

DATE 23 Aug

PAGE 3 OF 3

1	2	3	4	5	6	7	8
1 2 3 4 5 6 7 8 9	0 1 2 3 4 5 6 7 8 9	0 1 2 3 4 5 6 7 8 9	0 1 2 3 4 5 6 7 8 9	0 1 2 3 4 5 6 7 8 9	0 1 2 3 4 5 6 7 8 9	0 1 2 3 4 5 6 7 8 9	0 1 2 3 4 5 6 7 8 9
1, 1, 2, 3, 1	1, 1, 1, 1	1, 1, 1, 4, 8, 1	1, 1, 1, 1	1, 1, 1, 6, 7, 1	1, 1, 1, 1	2, 1, 1, 4, 1	1, 1, 1, 1
2, 1, 7, 8, 1	1, 1, 1, 1	1, 1, 1, 7, 8, 1	1, 1, 1, 1	1, 1, 1, 0, 3, 1	1, 1, 1, 1	1, 1, 1, 0, 3, 1	1, 1, 1, 1
. , 0, 2, 1, 4, 1	1, 1, 1, 1	. , 0, 1, 5, 9	1, 1, 1, 1	. , 0, 1, 2, 7	1, 1, 1, 1	. , 0, 0, 9, 8	1, 1, 1, 1
. , 0, 0, 7, 1, 1	1, 1, 1, 1	. , 0, 0, 6, 4	1, 1, 1, 1	. , 0, 0, 6	1, 1, 1, 1	. , 0, 0, 5, 6	1, 1, 1, 1
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. , 0, 0, 3, 9, 1	1, 1, 1, 1	. , 0, 0, 3, 8	1, 1, 1, 1	. , 0, 0, 3, 7	1, 1, 1, 1	. , 0, 0, 3, 6	1, 1, 1, 1
. , 0, 0, 3, 3, 1	1, 1, 1, 1	. , 0, 0, 3, 2	1, 1, 1, 1	. , 0, 0, 3, 1	1, 1, 1, 1	. , 0, 0, 3, 0	1, 1, 1, 1
. , 0, 0, 2, 8, 5	1, 1, 1, 1	. , 0, 0, 2, 8	1, 1, 1, 1	. , 0, 0, 2, 7, 8	1, 1, 1, 1	. , 0, 0, 2, 7, 6	1, 1, 1, 1
. , 0, 0, 2, 7, 1	1, 1, 1, 1	. , 0, 0, 2, 6, 8	1, 1, 1, 1	. , 0, 0, 2, 6, 6	1, 1, 1, 1	. , 0, 0, 2, 6, 4	1, 1, 1, 1
. , 0, 0, 2, 5, 8	1, 1, 1, 1	. , 0, 0, 2, 5, 6	1, 1, 1, 1	. , 0, 0, 2, 5, 4	1, 1, 1, 1	. , 0, 0, 2, 5, 2	1, 1, 1, 1
. , 0, 0, 2, 4, 7	1, 1, 1, 1	. , 0, 0, 2, 4, 7	1, 1, 1, 1	. , 0, 0, 2, 4, 7	1, 1, 1, 1	. , 0, 0, 2, 4, 7	1, 1, 1, 1
. , 0, 0, 2, 4, 7	1, 1, 1, 1	1, 1, 1, 1	1, 1, 1, 1	1, 1, 1, 1	1, 1, 1, 1	1, 1, 1, 1	1, 1, 1, 1
1 2 3 4 5 6 7 8 9	0 1 2 3 4 5 6 7 8 9	0 1 2 3 4 5 6 7 8 9	0 1 2 3 4 5 6 7 8 9	0 1 2 3 4 5 6 7 8 9	0 1 2 3 4 5 6 7 8 9	0 1 2 3 4 5 6 7 8 9	0 1 2 3 4 5 6 7 8 9
	1	2	3	4	5	6	7
							8

CROSS-SECTION SET #199

<u>Material</u>			<u>Group</u>	<u>Energy (keV)</u>
1. Sodium			1	3668
2. Stainless Steel			2	2225
3. U-238	300°K		3	1350
4. Pu-239	300°K	$\sigma_p = 370 \text{ b}$	4	825
5. U-238	2500°K		5	500
6. Pu-239	2500°K	$\sigma_p = 370 \text{ b}$	6	300
7. Oxygen			7	180
8. Carbon			8	110
9. Pu-239	300°K	$\sigma_p = 247 \text{ b}$	9	67
10. Pu-239	2500°K	$\sigma_p = 247 \text{ b}$	10	40.7
11. Pu-239	750°K	$\sigma_p = 247 \text{ b}$	11	25
12. Pu-239	1500°K	$\sigma_p = 247 \text{ b}$	12	15
13. U-238	750°K		13	9.1
14. U-238	1500°K		14	4
15. U-235	300°K	$\sigma_p = 126$	15	1
16. U-235	2500°K	$\sigma_p = 126$	16	0.3
17. Pu-239	750°K	$\sigma_p = 370$	17	0.1
18. Pu-239	1500°K	$\sigma_p = 370$	18	0.03
19. Aluminum				

LEGENDRE COEFFICIENT SET

<u>Material</u>	<u>Atomic Weight</u>	<u>Material</u>	<u>Atomic Weight</u>
1. Carbon	12.011	8. Chromium	52.010
2. Oxygen	16.000	9. Iron	55.840
3. Sodium	22.991	10. Stainless Steel	56.460
4. Sodium-1	23.000	11. Hastelloy	56.500
5. Sodium-2	23.010	12. Nickel	58.690
6. Aluminum	26.980	13. Niobium	92.910
7. Vanadium	50.950		

ON-LINE OUTPUT

RE 196 ELMOE
 S A M P L E P R O B L E M N O . 1
 IT. NO. 1 B SQUARE= 0.00200000 B= 0.04472136 SUM= 1.03785206
 IT. NO. 2 B SQUARE= 0.00241999 B= 0.04919349 SUM= 0.99872560
 IT. NO. 3 B SQUARE= 0.00240569 B= 0.04904783 SUM= 1.00001706
 IT. NO. 4 B SQUARE= 0.00240587 B= 0.04904975 SUM= 0.99999997

HOB0 EQUIVALENT
 IT. NO. 1 B SQUARE= 0.00200000 B= 0.04472136 SUM= 1.03794806
 IT. NO. 2 B SQUARE= 0.00241999 B= 0.04919349 SUM= 0.99872561
 IT. NO. 3 B SQUARE= 0.00240572 B= 0.04904819 SUM= 1.00001651
 IT. NO. 4 B SQUARE= 0.00240590 B= 0.04905004 SUM= 1.00000000

RE 196 ELMOE
 S A M P L E P R O B L E M N O . 2
 IT. NO. 1 B SQUARE= 0.00200000 B= 0.04472136 SUM= 1.03354345
 IT. NO. 2 B SQUARE= 0.00241999 B= 0.04919349 SUM= 0.99482176
 IT. NO. 3 B SQUARE= 0.00236151 B= 0.04859544 SUM= 1.00006440
 IT. NO. 4 B SQUARE= 0.00236223 B= 0.04860278 SUM= 1.00000012

HOB0 EQUIVALENT
 IT. NO. 1 B SQUARE= 0.00200000 B= 0.04472136 SUM= 1.03364480
 IT. NO. 2 B SQUARE= 0.00241999 B= 0.04919349 SUM= 0.99481191
 IT. NO. 3 B SQUARE= 0.00236157 B= 0.04859601 SUM= 1.00006203
 IT. NO. 4 B SQUARE= 0.00236226 B= 0.04860307 SUM= 1.00000010

RE 196 ELMOE
S A M P L E P R O B L E M N O . 1

OFF-LINE OUTPUT

MATERIAL CONSTANTS

MATERIAL	AT.WT	ATOMS/CC(E-24)	VOL.FRAC.	MATRIX FOR TRANSFORMING LEGENDRE EXPNS. COEFF.-CMS TO LAB			
				(1,1)	(1,2)	(1,3)	(1,4)
1	12.011000	1.00000000	-0.	0.99583E 00	-0.33149E-01	0.17588E-02	-0.11722E-03
2	16.000000	1.00000000	0.03120000	0.99765E 00	-0.24927E-01	0.98550E-03	-0.52205E-04
3	22.991000	1.00000000	0.00330000	0.99886E 00	-0.17371E-01	0.46996E-03	-0.19865E-04
4	56.460000	1.00000000	0.01525000	0.99975E 00	-0.80007E-02	0.87558E-04	-0.34335E-05
5	238.000000	1.00000000	0.01403999				
6	239.000000	1.00000000	0.00156000				
7	238.000000	1.00000000	-0.				
8	239.000000	1.00000000	-0.				
9	238.000000	1.00000000	-0.				
10	239.000000	1.00000000	-0.				

R= 0.98274157

OPTION 1

MATERIAL	CALCULATED	
	ALPHA	
1	0.2816316E-00	
2	0.2162987E-00	
3	0.1597795E-00	
4	0.6726708E-01	

MATERIAL DEPENDENT ELASTIC REMOVAL CROSS SECTION

GROUP

	1	2	3	4
2 -0.		0.7827E-02	0.1056E-02	0.1500E-02
3 -0.		0.1759E-01	0.9204E-03	0.1558E-02
4 -0.		0.3532E-01	0.2038E-02	0.3404E-02
5 -0.		0.2114E-01	0.1651E-02	0.2704E-02
6 -0.		0.4344E-01	0.2417E-02	0.2512E-02
7 -0.		0.2775E-01	0.2568E-02	0.3431E-02
8 -0.		0.2521E-01	0.1766E-02	0.3555E-02
9 -0.		0.2495E-01	0.2141E-02	0.3462E-02
10 -0.		0.2491E-01	0.2022E-02	0.4772E-02
11 -0.		0.2782E-01	0.2907E-02	0.4895E-02
12 -0.		0.2020E-01	0.1896E-02	0.8291E-02
13 -0.		0.2263E-01	0.2744E-02	0.6788E-02
14 -0.		0.1381E-01	0.4840E-02	0.5664E-02
15 -0.		0.6703E-02	0.4087E-03	0.2311E-02
16 -0.		0.5482E-02	0.3335E-03	0.2241E-02
17 -0.		0.4009E-02	0.2410E-03	0.1647E-02

MATERIAL

BUCKLING

INITIAL VALUE 0.20000000E-02
 FINAL VALUE 0.2405878E-02
 COARSE GROUP DATA

GROUP	FINE GROUP		FLUX	CURRENT/B	1/D	ELASTIC REMOVAL	ABSORPTION
	CORRESPONDENCE	0-					
1	0- 0	0.147416E 01	0.	0.	0.39255E-00		0.
2	1- 29	0.299984E 01	0.	0.	0.43178E-00	0.10383E-01	0.64480E-01
3	30- 58	0.433799E 01	0.	0.	0.50863E 00	0.20070E-01	0.48890E-01
4	59- 86	0.564262E 01	0.	0.	0.70405E 00	0.40758E-01	0.24633E-01
5	87-115	0.123874E 02	0.	0.	0.64267E 00	0.25496E-01	0.13707E-01
6	116-144	0.894581E 01	0.	0.	0.97859E 00	0.48365E-01	0.12802E-01
7	145-173	0.115149E 02	0.	0.	0.94079E 00	0.33751E-01	0.14007E-01
8	174-202	0.111647E 02	0.	0.	0.10140E 01	0.30528E-01	0.14613E-01
9	203-230	0.859068E 01	0.	0.	0.11142E 01	0.30551E-01	0.15775E-01
10	231-259	0.731513E 01	0.	0.	0.11639E 01	0.31708E-01	0.13817E-01
11	260-287	0.512522E 01	0.	0.	0.13713E 01	0.35618E-01	0.12710E-01
12	288-316	0.428785E 01	0.	0.	0.12465E 01	0.30383E-01	0.16420E-01
13	317-345	0.285616E 01	0.	0.	0.14256E 01	0.32166E-01	0.16621E-01
14	346-392	0.243306E 01	0.	0.	0.17734E 01	0.24311E-01	0.15216E-01
15	393-471	0.183030E 01	0.	0.	0.16978E 01	0.94224E-02	0.25014E-01
16	472-540	0.475049E-00	0.	0.	0.17987E 01	0.80564E-02	0.36893E-01
17	541-604	0.631634E-01	0.	0.	0.20865E 01	0.58966E-02	0.71235E-01
18	0- 0	0.558255E-02	0.	0.	0.40654E 01		0.

566	0.1936667	0.968735E-03	0.		0.208996E	01	0.132142E-02	0.32466E-03	0.18578E-04	0.
567	0.1903243	0.933240E-03	0.		0.208996E	01	0.127213E-02	0.31240E-03	0.18257E-04	0.
568	0.1870396	0.899282E-03	0.		0.208996E	01	0.122497E-02	0.30069E-03	0.17942E-04	0.
569	0.1838116	0.866838E-03	0.		0.208996E	01	0.117986E-02	0.28950E-03	0.17633E-04	0.
570	0.1806393	0.835820E-03	0.		0.208996E	01	0.113669E-02	0.27881E-03	0.17328E-04	0.
571	0.1775217	0.806137E-03	0.		0.208996E	01	0.109536E-02	0.26860E-03	0.17029E-04	0.
572	0.1744580	0.777715E-03	0.		0.208996E	01	0.105580E-02	0.25882E-03	0.16735E-04	0.
573	0.1711471	0.750489E-03	0.		0.208996E	01	0.101792E-02	0.24946E-03	0.16446E-04	0.
574	0.1684882	0.724397E-03	0.		0.208996E	01	0.981650E-03	0.24050E-03	0.16163E-04	0.
575	0.1655804	0.699387E-03	0.		0.208996E	01	0.946908E-03	0.23192E-03	0.15884E-04	0.
576	0.1627227	0.675406E-03	0.		0.208996E	01	0.913628E-03	0.22370E-03	0.15610E-04	0.
577	0.1599144	0.652410E-03	0.		0.208996E	01	0.881743E-03	0.21582E-03	0.15340E-04	0.
578	0.1571545	0.630357E-03	0.		0.208996E	01	0.851190E-03	0.20827E-03	0.15075E-04	0.
579	0.1544423	0.609205E-03	0.		0.208996E	01	0.821907E-03	0.20103E-03	0.14815E-04	0.
580	0.1517768	0.588915E-03	0.		0.208996E	01	0.793838E-03	0.19410E-03	0.14560E-04	0.
581	0.1491574	0.569451E-03	0.		0.208996E	01	0.766926E-03	0.18746E-03	0.14308E-04	0.
582	0.1465832	0.550775E-03	0.		0.208996E	01	0.741196E-03	0.18109E-03	0.14061E-04	0.
583	0.1440534	0.532853E-03	0.		0.208996E	01	0.716366E-03	0.17498E-03	0.13819E-04	0.
584	0.1415672	0.515648E-03	0.		0.208996E	01	0.692621E-03	0.16912E-03	0.13580E-04	0.
585	0.1391240	0.499129E-03	0.		0.208996E	01	0.669837E-03	0.16350E-03	0.13346E-04	0.
586	0.1367230	0.483265E-03	0.		0.208996E	01	0.647971E-03	0.15811E-03	0.13115E-04	0.
587	0.1343633	0.468026E-03	0.		0.208996E	01	0.626982E-03	0.15294E-03	0.12889E-04	0.
588	0.1320444	0.453384E-03	0.		0.208996E	01	0.606830E-03	0.14797E-03	0.12667E-04	0.
589	0.1297655	0.439312E-03	0.		0.208996E	01	0.587478E-03	0.14321E-03	0.12448E-04	0.
590	0.1275260	0.425786E-03	0.		0.208996E	01	0.56889CE-03	0.13863E-03	0.12233E-04	0.
591	0.1253251	0.412781E-03	0.		0.208996E	01	0.551033E-03	0.13423E-03	0.12022E-04	0.
592	0.1231622	0.400274E-03	0.		0.208996E	01	0.533874E-03	0.13001E-03	0.11815E-04	0.
593	0.1210366	0.388244E-03	0.		0.208996E	01	0.517381E-03	0.12595E-03	0.11611E-04	0.
594	0.1189477	0.376670E-03	0.		0.208996E	01	0.501526E-03	0.12205E-03	0.11410E-04	0.
595	0.1168948	0.365532E-03	0.		0.208996E	01	0.486280E-03	0.11830E-03	0.11213E-04	0.
596	0.1148774	0.354811E-03	0.		0.208996E	01	0.47116E-03	0.11469E-03	0.11020E-04	0.
597	0.1128948	0.344489E-03	0.		0.208996E	01	0.457510E-03	0.11123E-03	0.10830E-04	0.
598	0.1109464	0.334549E-03	0.		0.208996E	01	0.443936E-03	0.10789E-03	0.10643E-04	0.
599	0.1090317	0.324974E-03	0.		0.208996E	01	0.430872E-03	0.10468E-03	0.10459E-04	0.
600	0.1071500	0.315748E-03	0.		0.208996E	01	0.418295E-03	0.10160E-03	0.10279E-04	0.
601	0.1053007	0.306857E-03	0.		0.208996E	01	0.406184E-03	0.98622E-04	0.10101E-04	0.
602	0.1034834	0.298286E-03	0.		0.208996E	01	0.394519E-03	0.95760E-04	0.99269E-05	0.
603	0.1016974	0.290022E-03	0.		0.208996E	01	0.383281E-03	0.93003E-04	0.97556E-05	0.
604	0.0999423	0.282051E-03	0.		0.208996E	01	0.372452E-03	0.90347E-04	0.95872E-05	0.

HCBC EQUIVALENT

BUCKLING= 0.002406

GP	FLUX	FISSION SPECTRUM	NU SIGMA FISSION	3 SIGMA			INELASTICS			
				ABSORPTION	TRANSPORT	J TO J+1	2	3	4	5
1	1.474159	0.132000	0.037210	0.083414	0.392549	0.019192	0.012683	0.014027	0.011521	0.006949
2	2.999833	0.213000	0.033407	0.074863	0.431780	0.022990	0.010711	0.011885	0.008947	0.004764
3	4.337990	0.232000	0.025658	0.068959	0.508626	0.036066	0.016850	0.003768	0.000635	0.001376
4	5.642611	0.179000	0.009390	0.065391	0.704050	0.051440	0.005227	0.002350	0.000790	0.000395 -.
5	12.387383	0.116000	0.007876	0.039203	0.642674	0.033846	0.000263	0.000136	0.000040	0.000036 -.
6	8.945796	0.067000	0.007797	0.061168	0.978586	0.056270	0.000051	0.000019	0.000011	0.000006
7	11.514845	0.034000	0.007653	0.047758	0.940791	0.042497	0.000008	0.000000	0.000000	0.000002
8	11.164691	0.017000	0.007854	0.045141	1.014025	0.036071	0.002816	0.000002	0.000000	0.000000 -.
9	8.590661	0.010000	0.008171	0.046325	1.114185	0.036802	0.000899	0.000618	0.000000	-0. -0.
10	7.315114	0.	0.009048	0.045524	1.163945	0.034024	0.001067	0.000407	-0.	-0. -0.
11	5.125207	0.	0.009048	0.048328	1.371260	0.038205	0.000000	-0.	-0.	-0. -0.
12	4.287832	0.	0.010179	0.046803	1.246458	0.032923	-0.	-0.	-0.	-0. -0.
13	2.856148	0.	0.010179	0.048787	1.425600	0.034827	-0.	-0.	-0.	-0. -0.
14	2.433053	0.	0.011672	0.039527	1.773406	0.026971	-0.	-0.	-0.	-0. -0.
15	1.830296	0.	0.017598	0.034436	1.697826	0.012014	-0.	-0.	-0.	-0. -0.
16	0.475047	0.	0.034382	0.044949	1.798730	0.010409	-0.	-0.	-0.	-0. -0.
17	0.063163	0.	0.074646	0.077131	2.086463	0.008109	-0.	-0.	-0.	-0. -0.
18	0.005583	0.	0.069670	0.091154	4.065413	0.	0.	0.	0.	0. 0.

RE 196 ELMOE
S A M P L E P R O B L E M N O . 2

MATERIAL CONSTANTS

MATERIAL	AT.WT	ATOMS/CC(E-24)	VOL.FRAC.	MATRIX FOR TRANSFORMING LEGENDRE EXPNS. COEFF.-CMS TO LAB			
				(1,1)	(1,2)	(1,3)	(1,4)
1	12.011000	1.00000000	-0.	0.99583E 00	-0.33149E-01	0.17588E-02	-0.11722E-03
2	16.000000	1.00000000	0.03120000	0.99765E 00	-0.24927E-01	0.98550E-03	-0.52205E-04
3	22.991000	1.00000000	0.00330000	0.99886E 00	-0.17371E-01	0.46996E-03	-0.19805E-04
4	56.460000	1.00000000	0.01525000	0.99975E 00	-0.80007E-02	0.87558E-04	-0.34335E-05
5	238.000000	1.00000000	-0.				
6	239.000000	1.00000000	-0.				
7	238.000000	1.00000000	0.01403999				
8	239.000000	1.00000000	0.00156000				
9	238.000000	1.00000000	-0.				
10	239.000000	1.00000000	-0.				

R= 0.98274157

OPTION 1

MATERIAL	CALCULATED	
	ALPHA	
1	0.2816316E-00	
2	0.2162987E-00	
3	0.1597795E-00	
4	0.6726708E-01	

MATERIAL DEPENDENT ELASTIC REMOVAL CROSS SECTION

GROUP		MATERIAL		
	1	2	3	4
2 -0.		0.7829E-02	0.1056E-02	0.1501E-02
3 -0.		0.1759E-01	0.9204E-03	0.1558E-02
4 -0.		0.3532E-01	0.2039E-02	0.3405E-02
5 -0.		0.2115E-01	0.1652E-02	0.2705E-02
6 -0.		0.4344E-01	0.2417E-02	0.2512E-02
7 -0.		0.2776E-01	0.2569E-02	0.3432E-02
8 -0.		0.2521E-01	0.1766E-02	0.3556E-02
9 -0.		0.2495E-01	0.2142E-02	0.3463E-02
10 -0.		0.2492E-01	0.2022E-02	0.4773E-02
11 -0.		0.2782E-01	0.2907E-02	0.4896E-02
12 -0.		0.2019E-01	0.1895E-02	0.8288E-02
13 -0.		0.2263E-01	0.2743E-02	0.6785E-02
14 -0.		0.1374E-01	0.4817E-02	0.5635E-02
15 -0.		0.6497E-02	0.3957E-03	0.2234E-02
16 -0.		0.5218E-02	0.3170E-03	0.2126E-02
17 -0.		0.3792E-02	0.2279E-03	0.1557E-02

BUCKLING
 INITIAL VALUE 0.2000000E-02
 FINAL VALUE 0.2362230E-02
 COARSE GROUP DATA

GROUP	FINE GROUP CORRESPONDENCE	FLUX	CURRENT/B	1/D	ELASTIC REMOVAL	ABSORPTION
1	0 - 0	0.147599E 01	0.	0.39255E-00	0.10385E-01	0.64480E-01
2	1- 29	0.300395E 01	0.	0.43176E-00	0.20069E-01	0.48890E-01
3	30- 58	0.434479E 01	0.	0.50862E 00	0.40760E-01	0.24633E-01
4	59- 86	0.565207E 01	0.	0.70404E 00	0.64267E 00	0.13707E-01
5	87-115	0.124196E 02	0.	0.97857E 00	0.48369E-01	0.12802E-01
6	116-144	0.897294E 01	0.	0.94079E 00	0.33759E-01	0.14007E-01
7	145-173	0.115559E 02	0.	0.10140E 01	0.30537E-01	0.14613E-01
8	174-202	0.112124E 02	0.	0.11142E 01	0.30559E-01	0.15775E-01
9	203-230	0.863374E 01	0.	0.11639E 01	0.31716E-01	0.13817E-01
10	231-259	0.735728E 01	0.	0.13713E 01	0.35626E-01	0.12710E-01
11	260-287	0.515829E 01	0.	0.12464E 01	0.30372E-01	0.16490E-01
12	288-316	0.431398E 01	0.	0.14256E 01	0.32155E-01	0.16692E-01
13	317-345	0.287096E 01	0.	0.17735E 01	0.24195E-01	0.15595E-01
14	346-392	0.243074E 01	0.	0.17010E 01	0.91263E-02	0.26351E-01
15	393-471	0.177067E 01	0.	0.17981E 01	0.76611E-02	0.39950E-01
16	472-540	0.424069E-00	0.	0.20863E 01	0.55761E-02	0.77833E-01
17	541-604	0.502290E-01	0.	0.40654E 01	0.	
18	0 - 0	0.391853E-02	0.			

566	0.1936667	0.755530E-03	0.	0.208996E 01	0.103889E-02	0.25608E-03	0.16584E-04	0.
567	0.1903243	0.726314E-03	0.	0.208996E 01	0.997834E-03	0.24582E-03	0.16298E-04	0.
568	0.1870396	0.698458E-03	0.	0.208996E 01	0.958698E-03	0.23605E-03	0.16017E-04	0.
569	0.1838116	0.671933E-03	0.	0.208996E 01	0.921380E-03	0.22675E-03	0.15740E-04	0.
570	0.1806393	0.646656E-03	0.	0.208996E 01	0.885787E-03	0.21790E-03	0.15469E-04	0.
571	0.1775217	0.622545E-03	0.	0.208996E 01	0.851830E-03	0.20947E-03	0.15202E-04	0.
572	0.1744580	0.599532E-03	0.	0.208996E 01	0.819428E-03	0.20143E-03	0.14939E-04	0.
573	0.1714471	0.577756E-03	0.	0.208996E 01	0.785504E-03	0.19375E-03	0.14682E-04	0.
574	0.1684882	0.556561E-03	0.	0.208996E 01	0.758984E-03	0.18643E-03	0.14428E-04	0.
575	0.1655804	0.536496E-03	0.	0.208996E 01	0.730799E-03	0.17944E-03	0.14179E-04	0.
576	0.1627227	0.517314E-03	0.	0.208996E 01	0.703885E-03	0.17276E-03	0.13934E-04	0.
577	0.1599144	0.498973E-03	0.	0.208996E 01	0.678178E-03	0.16638E-03	0.13694E-04	0.
578	0.1571545	0.481434E-03	0.	0.208996E 01	0.653620E-03	0.16029E-03	0.13458E-04	0.
579	0.1544423	0.464661E-03	0.	0.208996E 01	0.630154E-03	0.15447E-03	0.13225E-04	0.
580	0.1517768	0.448616E-03	0.	0.208996E 01	0.607726E-03	0.14890E-03	0.12997E-04	0.
581	0.1491574	0.433266E-03	0.	0.208996E 01	0.586287E-03	0.14359E-03	0.12773E-04	0.
582	0.1465832	0.418578E-03	0.	0.208996E 01	0.565787E-03	0.13851E-03	0.12552E-04	0.
583	0.1440534	0.404520E-03	0.	0.208996E 01	0.546180E-03	0.13365E-03	0.12336E-04	0.
584	0.1415672	0.391061E-03	0.	0.208996E 01	0.527423E-03	0.12901E-03	0.12123E-04	0.
585	0.1391240	0.378171E-03	0.	0.208996E 01	0.509475E-03	0.12457E-03	0.11914E-04	0.
586	0.1367230	0.365824E-03	0.	0.208996E 01	0.492296E-03	0.12031E-03	0.11708E-04	0.
587	0.1343633	0.353991E-03	0.	0.208996E 01	0.475850E-03	0.11625E-03	0.11506E-04	0.
588	0.1320444	0.342650E-03	0.	0.208996E 01	0.460100E-03	0.11235E-03	0.11307E-04	0.
589	0.1297655	0.331775E-03	0.	0.208996E 01	0.445015E-03	0.10862E-03	0.11112E-04	0.
590	0.1275260	0.321346E-03	0.	0.208996E 01	0.430560E-03	0.10505E-03	0.10920E-04	0.
591	0.1253251	0.311342E-03	0.	0.208996E 01	0.416708E-03	0.10163E-03	0.10732E-04	0.
592	0.1231622	0.301741E-03	0.	0.208996E 01	0.403428E-03	0.98349E-04	0.10547E-04	0.
593	0.1210366	0.292526E-03	0.	0.208996E 01	0.390694E-03	0.95205E-04	0.10365E-04	0.
594	0.1189477	0.283678E-03	0.	0.208996E 01	0.378479E-03	0.92191E-04	0.10186E-04	0.
595	0.1168948	0.275181E-03	0.	0.208996E 01	0.366760E-03	0.89300E-04	0.10010E-04	0.
596	0.1148774	0.267018E-03	0.	0.208996E 01	0.355513E-03	0.86527E-04	0.98373E-05	0.
597	0.1128948	0.259172E-03	0.	0.208996E 01	0.344715E-03	0.83865E-04	0.96675E-05	0.
598	0.1109464	0.251631E-03	0.	0.208996E 01	0.334346E-03	0.81311E-04	0.95007E-05	0.
599	0.1090317	0.244379E-03	0.	0.208996E 01	0.324385E-03	0.78858E-04	0.93367E-05	0.
600	0.1071500	0.237404E-03	0.	0.208996E 01	0.314815E-03	0.76501E-04	0.91756E-05	0.
601	0.1053007	0.230692E-03	0.	0.208996E 01	0.305616E-03	0.74237E-04	0.90172E-05	0.
602	0.1034834	0.224232E-03	0.	0.208996E 01	0.296771E-03	0.72062E-04	0.88616E-05	0.
603	0.1016974	0.218012E-03	0.	0.208996E 01	0.288265E-03	0.69970E-04	0.87087E-05	0.
604	0.0999423	0.212022E-03	0.	0.208996E 01	0.280081E-03	0.67958E-04	0.85584E-05	0.

HC80 EQUIVALENT

BUCKLING= 0.002362

GP	FLUX	FISSION		NU SIGMA	3 SIGMA			INELASTICS						
		SPECTRUM	FISSION		ABSORPTION	TRANSPORT	J	TC	J+1	2	3	4	5	6
1	1.475992	0.132000	0.037210	0.083414	0.392549	0.019192	0.012683	0.014027	0.011521	0.006949	0.005720			
2	3.003948	0.213000	0.033407	0.074865	0.431765	0.022993	0.010711	0.011885	0.008947	0.004764	0.003852			
3	4.344786	0.232000	0.025658	0.068959	0.508622	0.036065	0.016850	0.003768	0.000635	0.001376	0.000189			
4	5.652061	0.179000	0.009390	0.065393	0.704041	0.051443	0.005227	0.002350	0.000790	0.000395	-0.			
5	12.419576	0.116000	0.007876	0.039214	0.642669	0.033858	0.000263	0.000136	0.000040	0.000036	-0.			
6	8.972924	0.067000	0.007797	0.061171	0.978570	0.056274	0.000051	0.000019	0.000011	0.000006	0.000005			
7	11.555861	0.034000	0.007653	0.047767	0.940792	0.042506	0.000008	0.000000	0.000000	0.000000	0.000002			
8	11.212336	0.017000	0.007854	0.045150	1.014016	0.036079	0.002816	0.000002	0.000000	0.000000	-0.			
9	8.633724	0.010000	0.008171	0.046333	1.114180	0.036810	0.000899	0.000618	0.000000	-0.	-0.			
10	7.357265	0.	0.009048	0.045533	1.163943	0.034032	0.001067	0.000407	-0.	-0.	-0.			
11	5.158281	0.	0.009048	0.048336	1.371255	0.038213	0.000000	-0.	-0.	-0.	-0.			
12	4.313967	0.	0.010179	0.046862	1.246432	0.032912	-0.	-0.	-0.	-0.	-0.			
13	2.870952	0.	0.010179	0.048847	1.425599	0.034816	-0.	-0.	-0.	-0.	-0.			
14	2.430732	0.	0.011672	0.039790	1.773461	0.026855	-0.	-0.	-0.	-0.	-0.			
15	1.770665	0.	0.017689	0.035477	1.701016	0.011717	-0.	-0.	-0.	-0.	-0.			
16	0.424068	0.	0.035332	0.047611	1.798076	0.010014	-0.	-0.	-0.	-0.	-0.			
17	0.050229	0.	0.079622	0.083409	2.086336	0.007788	-0.	-0.	-0.	-0.	-0.			
18	0.003919	0.	0.076456	0.099250	4.065413	0.	0.	0.	0.	0.	0.			

ARGONNE NATIONAL LAB WEST



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